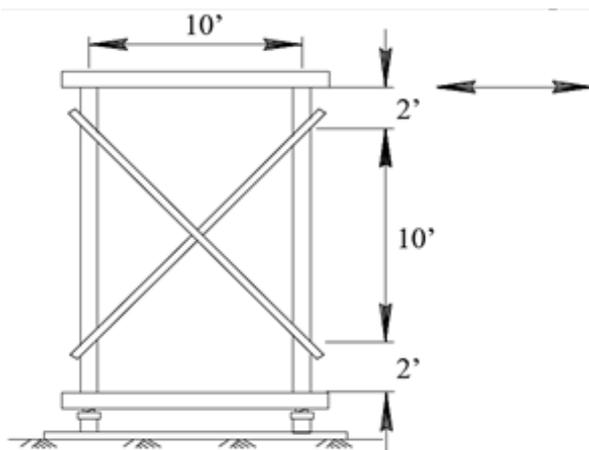


Appendix D Example 14 – Diagonal Bracing of Single Tier Framed Bent – Nailed Connections

Refer to *Falsework Manual*, Section 6-3, *Diagonal Bracing* and Section 5-3, *Timber Fasteners*. This example demonstrates how to determine if the bracing system of a single tier framed bent is adequate. All connections are nailed.

Given Information



2% Dead Load = 1900 lb
Wind Load = 1800 lb

Posts:
12 x 12 Rough Douglas Fir-Larch #1
(G=0.50)

Diagonal Braces:
2x8 Douglas Fir-Larch #2 (G=0.50)

Connectors:
Brace to Post 10-20d common nails
Intersection of Brace 4-16d common nails

Figure D-14-1. Single Tier Framed Bent with Diagonal Bracing

Determine if the Bracing System is Adequate

1. Determine the connection capacity between the brace and post:

10-20d Common Wire Nails

Length = 4"

Diameter (D) = 0.192"

Penetration = 4" - 1.5" = 2.5"

Minimum penetration for full tabular value = 10D = 10(0.192") = 1.92"

Minimum penetration = 6D = 6(0.192") = 1.15"

Reference lateral design value (Z) from NDS table 12N = 170 lb

Adjustment factors from NDS Table 11.3.1:

$C_D = 1.25$	<i>Duration Factor for 2% lateral loading</i>
$C_M = 1.0$	<i>Wet Service Factor NDS 11.3.3 (Assume < 19% moisture content)</i>
$C_t = 1.0$	<i>Temperature Factor NDS 11.3.4 (Temp up to 100°F)</i>
$C_g = 1.0$	<i>Group Action Factor NDS 11.3.6</i>
$C_{\Delta} = 1.0$	<i>Geometry Factor NDS 12.5.1</i>
$C_{eg} = 1.0$	<i>End Grain Factor NDS 12.5.2</i>
$C_{di} = 1.0$	<i>Diaphragm Factor NDS 12.5.3</i>
$C_{tn} = 1.0$	<i>Toe Nail Factor NDS 12.5.4</i>

Adjusted lateral design value $Z' = Z(C_D)(C_M)(C_t)(C_g)(C_{\Delta})(C_{eg})(C_{di})(C_{tn}) = 213 \text{ lb}$

Connection capacity = $nZ' = 10(213 \text{ lb}) = 2130 \text{ lb}$ (n equals number of nails)

2. Determine the capacity of the diagonal brace in tension:

Reference design value in tension $F_t = 575 \text{ psi}$ (NDS supplement table 4A)

Adjustment factors from NDS table 4.3.1:

$C_D = 1.25$	<i>Duration Factor for 2% lateral loading</i>
$C_M = 1.0$	<i>Wet Service Factor NDS table 4A (Assume < 19% moisture content)</i>
$C_t = 1.0$	<i>Temperature Factor NDS table 2.3.3 (Temp up to 100°F)</i>
$C_F = 1.2$	<i>Size Factor NDS Table 4A</i>
$C_i = 1.0$	<i>Incising Factor NDS 4.3.8</i>

Adjusted design value $F_t' = F_t (C_D)(C_M)(C_t)(C_F)(C_i) = 863 \text{ psi}$

Tension capacity = $863 \text{ psi}(1.5'')(7.25'') = 9385 \text{ lb}$

3. Determine the strength value of the tension members:

$9385 \text{ lb} > 2130 \text{ lb} \quad \therefore$ Connection strength controls

4. Calculate the horizontal component of the strength value for the tension members

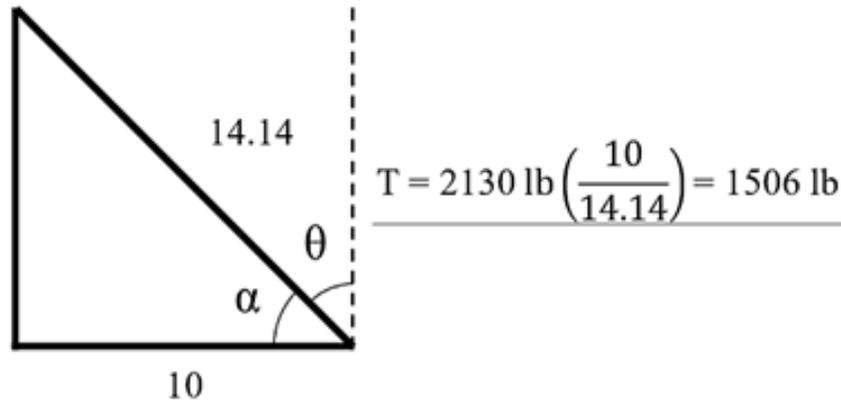


Figure D-14-2. Geometric Components of Tension Strength Value

5. Determine the capacity of diagonal brace in compression:

First check adequacy of the connection to reduce the unsupported length of compression member (See section 6-3.02 Wood cross bracing):

4-16d Common Wire Nails

Reference withdrawal design value $W = 40$ lb/inch of penetration (NDS table 12.2C)

Adjustment factors from NDS Table 11.3.1:

- $C_D = 1.25$ *Duration Factor for 2% lateral loading*
- $C_M = 1.0$ *Wet Service Factor NDS 11.3.3 (Assume < 19% moisture content)*
- $C_t = 1.0$ *Temperature Factor NDS 11.3.4 (Temp up to 100°F)*
- $C_{eg} = 1.0$ *End Grain Factor NDS 12.5.2*
- $C_{tn} = 1.0$ *Geometry Factor NDS 12.5.4*

Adjusted withdrawal design value $W' = W(C_D)(C_M)(C_t)(C_{eg})(C_{tn}) = 50$ lb/inch

Penetration $p = 1.5$ "

Connection capacity = $n(p)(Z') = 4(1.5)(50 \text{ lb/inch}) = 300$ lb (n equals number of nails)

$300 \text{ lb} > 250 \text{ lb}$ (minimum required per section 6-3.02)

Check cross brace capacity in compression:

Reference design value in compression $F_c = 1350$ psi (NDS supplement table 4A)

Adjustment factors from NDS table 4.3.1:

$C_D = 1.25$ *Duration Factor for 2% lateral loading*

$C_M = 1.0$ *Wet Service Factor NDS table 4A (Assume < 19% moisture content)*

$C_t = 1.0$ *Temperature Factor NDS table 2.3.3 (Temp up to 100°F)*

$C_F = 1.05$ *Size Factor NDS Table 4A*

$C_i = 1.0$ *Incising Factor NDS 4.3.8*

$C_P = 0.083$ *Column Stability Factor NDS 3.7.1 (unsupported length = $\frac{14.14}{2} = 7.07'$)*

Adjusted design compression value $F_c' = F_c (C_D)(C_M)(C_t)(C_F)(C_i)(C_P) = 147$ psi

Compression brace capacity = 147 psi (1.5")(7.25") = 1599 lb

6. Determine the strength value of the compression members:

Connection capacity = 2130 lb

(See step 1. Capacity in tension and compression are the same)

1599 lb < 2130 lb ∴ 2x8 brace controls compression

Limit to ½ theoretical strength for compression values: See section 6-3.02, *Wood Cross Bracing*.

Reduced compression brace capacity = $\frac{1599 \text{ lb}}{2} = 800$ lb

7. Calculate the horizontal component of the strength value for the compression member:

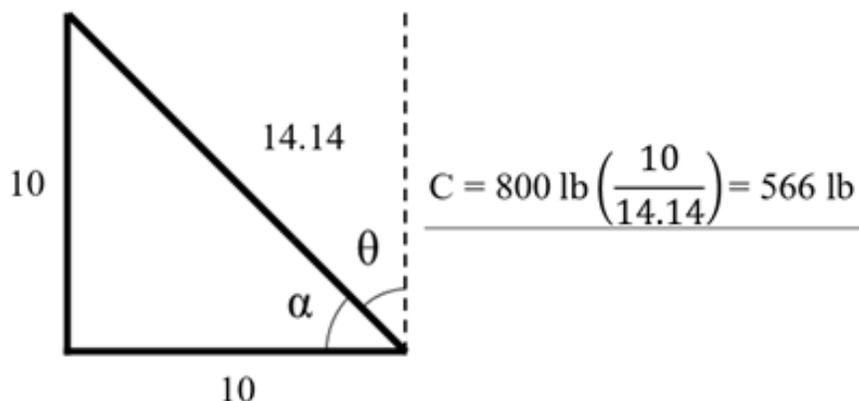


Figure D-14-3. Geometric Components of Compression Strength Value

8. Calculate the total resisting capacity of the diagonal bracing system:

Summarize Result for 2% Dead Load

Total resisting capacity = C + T = 566 lb + 1506 lb = 2072 lb

Resisting Capacity = 2072 lb > Horizontal Demand Force = 1900 lb

Bracing system is adequate for 2% Dead Load

Summarize Result for Wind Load

Repeat above process for wind load to calculate the Resisting Capacity, using $C_D = 1.6$ rather than 1.25. All other factors are the same.

The Resisting Capacity for wind load can also be derived by multiplying the resisting capacity for 2% Dead Load (above) by the ratio $\frac{C_D \text{ wind}}{C_D \text{ 2\%}} = \frac{1.6}{1.25}$

Resisting Capacity = 2072 lb $\left(\frac{1.6}{1.25}\right)$ = 2652 lb > Horizontal Demand Force = 1800 lb

Bracing system is adequate for Wind Load