Conventional Retaining Walls

This module presents the Caltrans standard practice for the geotechnical investigation, design, and reporting for conventional retaining walls. Conventional retaining walls are rigid gravity and semi-gravity retaining walls as defined in AASHTO LRFD BDS Section 11.2. Conventional retaining walls are reinforced concrete walls in the shape of an “L” or inverted “T”. Conventional retaining walls commonly used by Caltrans are Retaining Wall Types 1, 5, and 6 as detailed in the Caltrans Standard Plans and Caltrans Revised Standard Plans, and Retaining Wall Type 7 as detailed in the Caltrans Bridge Standard Detail Sheets. Conventional retaining walls are also any variation or modification of these retaining walls that may include piles, sound walls, barriers, or enlarged foundations.

In addition to this module, the documents that guide or govern the investigation, design, and reporting for conventional retaining walls include:

- AASHTO LRFD Bridge Design Specifications, 2012 (Sixth Edition) with California Amendments
- Caltrans Standard Plans and Revised Standard Plans
- Caltrans Memo to Designers (MTD) 5-19, Earth Retaining Systems Communication
- Caltrans Geotechnical Manual, Soil Correlations
- Caltrans Geotechnical Manual, Foundation Reports for Earth Retaining Systems
- Caltrans Geotechnical Manual, Geotechnical Design Reports

Retaining wall types detailed in the Caltrans Standard Plans are commonly designed through a coordinated effort between the Geoprofessional and District Design Engineer; however, upon special arrangement, Structure Design or consultant engineers may act in place of the District Design Engineer. Retaining Wall Type 7 and varied or modified Standard Plan retaining walls are designed through a coordinated effort between the Geoprofessional and Structure Design or consultant engineers.

The Geoprofessional assists in all phases of project development as requested by District or Structure Design. This assistance may include research, preliminary retaining wall design, and type selection during the project planning or early design phase; field investigation, analyses, external retaining wall design, and design support during the project design phase; and construction support and possible retaining wall alterations due to project changes or unforeseen conditions discovered during the construction phase. The geotechnical effort must be documented and communicated in appropriate reports and memorandum.
Conventional retaining walls are typically type-selected during project planning or early design phases through the coordinated effort between the Geoprofessional and project development staff. A more formal type selection process may be conducted for some retaining walls, as may occur for complex projects or wall sites. In such cases, the type selection should be based on preliminary geotechnical reports addressing the retaining walls. A thorough discussion of retaining wall type selection may be found in Chapter 10 of the Federal Highway Administration Publication No. FHWA-NHI-07-071, *Earth Retaining Structures Reference Manual.*

**Investigations**

A geotechnical investigation must be conducted for all retaining walls. The goal of the geotechnical investigation for conventional retaining walls is to determine the distribution, properties, and behavior of the soil and rock that will affect retaining wall design and construction; the groundwater condition that will affect retaining wall design and construction; the distribution of unsuitable or weak materials requiring remedial measures; and the suitability of excavated soil to be used as embankment fill or structure backfill. In addition to permanent features, the investigation should gather data useful in the evaluation of temporary construction features such as excavations and shoring.

The geotechnical investigation should provide data to determine the:

- strength and settlement characteristics of foundation soils
- strength and weight of soils to be retained
- strength and unit weight of soils affecting slope stability
- corrosion potential of soils in contact with the retaining wall
- groundwater location
- quantity of groundwater seepage

All foundation soils, including recently placed engineered fills, should be investigated.

Refer to the *Geotechnical Investigations* module for direction on performing a literature search. In some instances, the information obtained through the literature search and field mapping may be sufficient for retaining wall design. Examples of such instances are walls built in “layer cake” sedimentary strata where nearby borings exist for the same sedimentary units, or walls founded on rock with abundant rock exposures and previous testing is adequate to sufficiently characterize the rock.

The Geoprofessional should develop a prudent exploration plan in light of site constraints and available resources, and consider uncertainty and risk of not drilling at a particular location. The Geoprofessional should:
• Obtain retaining wall layout and configuration as accurately as possible. Final wall layout and height may not be determined until late in the design phase.

• Perform a literature search. Gather all relevant information related to site geology, strength of soils, and geologic hazards.

• Perform geologic field mapping of the wall site. The mapping should be sufficient to generate geologic cross sections along the retaining wall when combined with other terrain data.

• Develop a subsurface exploration and lab testing plan to augment information gathered through archive research and field mapping. Locate exploratory borings, CPT, and/or drive holes spaced at maximum intervals of 100 to 200 feet along the proposed wall alignment, with borings strategically positioned in front, behind, and directly on the retaining wall layout line. The number of borings necessary to delineate site conditions may be greatly reduced or increased due to the value of pre-existing data, uniformity of site geology, and the quality of site specific geologic mapping.

• Advance the subsurface exploration to an appropriate depth. The depth of exploration should generally extend below the foundation to the deepest of:
  o 15 feet,
  o twice the height of the retaining wall,
  o 4 times the estimated footing width,
  o to the full depth of soft, loose, weak soils upon which wall stability and settlement is dependent, or
  o to a depth below where material strength and strain characteristics are acceptable.

• Conduct SPT at maximum depth intervals of 5 feet. Closer intervals of SPT testing should be considered within a depth of 2 times the footing width below the proposed bottom of footing (the zone of greatest bearing pressure), and where soil strength properties are projected to be low and highly varied such as poorly compacted fill or soft/loose alluvial soils.

• Anticipate relatively deep exploration for retaining walls on piles, retaining walls with ground anchors, and retaining walls founded over soils that are loose, soft, or otherwise weak.

• Gather data to evaluate the stability of permanent and temporary excavations and cut slopes that will influence design and construction of the retaining wall. In rock and intermediate geomaterial, rock cores and down-hole tele-viewing can yield useful information on rock quality and joint orientation. All material within the active wedge must meet the minimum strength assumed for structure backfill (friction angle, phi = 34 degrees).

• Estimate soil strengths based on index properties established through SPT, pocket penetrometer, torvane, and CPT (see Correlations Module). For retaining walls founded on IGM or rock, strengths may be sufficiently estimated by reviewing data developed for similar rock on nearby projects. Perform laboratory strength
tests only when correlation-based strengths result in borderline acceptable or unacceptable calculation results.

- Conduct consolidation testing of clay soils wherever settlement magnitude and rate are significant project considerations.
- Conduct corrosion testing on representative samples of the soil that will contact the retaining wall. The Geoprofessional should review, evaluate, and interpret the collected data to arrive at reasonable assessments of corrosion potential. For example, if some samples gathered from a single sedimentary stratum or formational unit are found to be corrosive and other samples are found to be non-corrosive, the entire sedimentary stratum or formational unit should be deemed corrosive. If only a small zone of a formational unit appears to be corrosive, the Geoprofessional should attempt to ascertain why only that zone should be regarded as corrosive.
- Sample and test mandatory borrow sites to determine if the material satisfies corrosion and gradation criteria for structure backfill. Sample and test project cut excavations to determine if material generated on-site will meet structure backfill requirements and should be designated for use as such. Conventional retaining walls may be constructed atop fills that do not exist at the time of the investigation but will be placed during the project. If the material borrow site is known the site should be investigated to determine soil properties useful in further evaluations.

**Design**

The design of conventional retaining wall must follow the Geotechnical Manual and AASHTO LRFD BDS. The design must address strength, service, and extreme event limit states.

The walls in the Standard Plan and Bridge Standard Detail sheets have been designed for sliding, deflection, eccentricity and internal structural stability requirements for the specific retained and foundation soil strengths listed on the plan sheets. The geoprofessional must evaluate the site soils to determine if the conditions meet the minimum strength and stability criteria provided on the Standard Plan and the Bridge Standard Detail sheets.

The geotechnical design of a conventional retaining wall should include:

- Development of the Design Soil/Rock Profile
- Calculation of the Factored Gross Nominal Bearing Resistances (Strength and Extreme Event Limit States)
- Determination of frictional resistance of foundation material for sliding analysis
- Calculation of the Total and differential settlement
- Evaluation of overall slope stability (Service and Extreme Event Limit States)
- Evaluation of erosion susceptibility and mitigation
• Evaluation of seismic stability
• Design of surface and subsurface drainage systems
• Design of foundation improvement requirements
• Determination of the minimum unbonded ground anchor length for Type 7 walls that incorporate ground anchors

Design Soil Profile

Use the available geologic information to develop a design soil profile along the wall layout line. The stratigraphy should be presented in the following format (ref: Foundation Reports for Earth Retaining Systems).

<table>
<thead>
<tr>
<th>Layer No.</th>
<th>Layer Boundaries</th>
<th>Group Name</th>
<th>Engineering Parameters</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Finished grade to elev. 300</td>
<td>Silty Sand (fill)</td>
<td>$\phi' = 34 \text{ degrees}, \gamma = 120 \text{ pcf}$</td>
</tr>
<tr>
<td>2</td>
<td>Elev. 285 to 300</td>
<td>Silty Sand</td>
<td>$\phi' = 33 \text{ degrees}, \gamma = 113 \text{ pcf}$</td>
</tr>
<tr>
<td>3</td>
<td>Elev. 272 to 285</td>
<td>Poorly-graded Sand</td>
<td>$\phi' = 34 \text{ degrees}, \gamma = 120 \text{ pcf}$</td>
</tr>
<tr>
<td>4</td>
<td>Elev. 250 to 272</td>
<td>Silty Sand</td>
<td>$\phi' = 34 \text{ degrees}, \gamma = 114 \text{ pcf}$</td>
</tr>
</tbody>
</table>

The stratigraphy may also be presented graphically on a geologic profile.

Factored Gross Nominal Bearing Resistance (Strength and Extreme Event Limit States)

The Factored Gross Nominal Bearing Resistance must be calculated for soil foundations for both the Strength Limit State and Extreme Limit State. The bearing resistance is affected when groundwater is at a depth less than 1.5 times the footing width below the footing base. Determine the bearing resistance using the highest anticipated groundwater level at the footing location according to AASHTO LRFD BDS Section 10.6.3.

For bearing resistance on rock follow the design procedures in AASHTO LRFD BDS Section 10.6.3.2. For competent foundation rock types, it may not be necessary to calculate the Factored Gross Nominal Bearing Resistance, per AASHTO LRFD BDS Section 10.6.3.2.

The Spread Footing Data Table must follow the Foundation Reports for Earth Retaining Systems (FR for ERS).
Walls on Slopes

The proximity of a retaining wall footing to a descending slope must be considered in the bearing resistance calculations. If the finished ground in front of the retaining wall toe slopes downward within a distance that is twice the width of the footing measured from the retaining wall toe, then the bearing resistance will differ from the level ground configuration.

The Modified Bearing Capacity Factors for Footing Adjacent to Sloping Ground (AASHTO LRFD BDS 10.6.3.1.2c) developed by Meyerhof (1957), or similar, must be used. Table C11.10.2.2.1 in the AASHTO LRFD Bridge Design Specifications provides guidelines for minimum foundation embedment when a wall is located on a slope.

Additionally, a sliding analysis using the retaining wall configuration and the foundation soil characteristics must be conducted. Because the site geometry does not conform to the Standard Plans and Standard Details, the PS&E must be prepared by Structure Design. The sliding analysis will be performed by the Structure Designer. The Structure Designer may request assistance from Geotechnical Services with calculating the factored sliding resistance. See AASHTO LRFD BDS section 10.6.3.4.

Settlement Evaluation (Service Limit State)

Calculate settlement using the net bearing stress shown in the Standard Plans, Revised Standard Plans, Standard Details, or provided by the Structure Designer. If the calculated settlement is less than or equal to the specified permissible settlement, the retaining wall geometry and configuration meet the Service Limit State settlement criteria. If the calculated settlement exceeds the permissible settlement, then the retaining wall must be redesigned or the foundation conditions improved.

Settlement must be calculated per AASHTO LRFD Bridge Design Specifications section 10.6.2.4. The total settlement may include elastic, consolidation and secondary components. Settlements must be within the tolerable criteria for the type of retaining wall selected. The settlement must be calculated for the Service Limit State stress. The settlement evaluation must include settlement that occurs during and after wall construction.

Tolerable total and differential settlement criteria are as follows:

<table>
<thead>
<tr>
<th>Wall Type</th>
<th>Tolerable Total Settlement</th>
<th>Differential Settlement over a Distance of 100 feet</th>
</tr>
</thead>
<tbody>
<tr>
<td>Conventional Retaining Wall</td>
<td>≤ 1” or ≤ 2”</td>
<td>≤ 0.75”</td>
</tr>
</tbody>
</table>
More stringent tolerances may be necessary to meet aesthetic requirements for the walls.

Settlement evaluation for foundations on rock must follow the recommendations in AASHTO LRFD BDS Section 10.6.2.4.4.

Foundation stress distribution that may affect underground utilities or adjacent structure evaluation will be provided by the Geoprofessional upon request by the Structure Designer or other stakeholders such as utility owners or the District Design Engineer.

**Sliding Evaluation**

The Standard Plan and Standard Detail wall designs have been evaluated for sliding using a foundation soil friction angle of 34 degrees and a fully developed passive resistance on the vertical face of the footing toe and shear key. If the retaining wall is founded on soil or rock with frictional resistance less than 34 degrees, then the site conditions do not conform to those assumed for the preparation of the Standard Plans and Standard Details. The Structure Designer should be notified that sliding resistance analyses for strength and extreme event limit states are required. This analysis is the responsibility of the Structure Designer. The Structure Designer may request assistance calculating the factored sliding resistance.

**Overall Slope Stability (Service and Extreme Event Limit States)**

The overall stability of the wall must be calculated using Service I Loads and AASHTO LRFD BDS Section 11.6.2.3.

**Erosion Susceptibility and Mitigation**

Embedment of the retaining wall foundation must account for anticipated scour, erosion or undermining. AASHTO LRFD BDS Sections 2.6.4.4.2 and 10.6.1.2 must be followed. Considerations for embedment should include slope geometry, erosional potential in front of the wall, frost heave protection, future construction activities, and external and global wall stability.

When the foundation material is subject to erosion or scour, measures must be taken to avoid undermining. In this instance the embedment may exceed the minimum embedment depth requirements, and additional countermeasures such as erosion control and hard facing should be considered.

Depending on the type of conventional retaining wall, the minimum cover for footings if scour or freezing is not of concern is 1.5 or 2 feet.
Seismic Stability

Standard Plan Retaining Wall site seismic criteria threshold must be analyzed to confirm that the Coefficient of Horizontal Acceleration, \( k_h \), does not exceed 0.2. The \( k_h \) is calculated as 1/3 Peak Ground Acceleration (PGA). Therefore, at sites where the PGA is equal to or less than 0.6g the Standard Plans are applicable. If the site seismic criteria cannot be met the wall will require a site-specific design by Structure Design.

Seismic recommendations must also address seismic hazards such as liquefaction impacts to bearing resistance, overall stability and lateral deflection. The maximum allowable displacements are governed by wall performance and potentially-impacted facilities.

Surface and Subsurface Drainage Systems

Drainage must be provided for all walls. If wall drainage cannot be provided, the wall design must include hydrostatic pressure.

Additional drainage measures should be implemented if the wall backfill cannot be depended on to be fully drained or if the groundwater conditions at the project site will affect the integrity of the wall. These additional groundwater control measures may include deep underdrains and horizontal drains in addition to geocomposite drains, underdrains and drainage blankets at the wall or at the back of the backfill. To the greatest extent possible these groundwater control measures should be located in a manner to prevent the infiltration of groundwater into the structure backfill.

Surface drainage should be directed away from the wall. If this is not possible, surface drainage appurtenances such as impervious drainage inlets, lined ditches, curbs and gutters should be recommended.

As a general rule, infiltration basins should not be positioned so as to introduce water into the retained earth zone or into the foundation material. The effects of bioswales in the vicinity of earth retention systems should be carefully considered. Depending upon the details of their construction, bioswales may lead to increased infiltration of water. The possibility of increased hydrostatic pressure and soil pore pressures should be considered.

Modified Design of Conventional Retaining Walls

The geoprofessional must review the proposed retaining wall configuration for conformance with the Standard Plans and Standard Details. Among the important configuration elements to check are the lateral distance to a descending slope in front of the retaining wall, the vertical footing cover, the ground slope in the retained zone, additional surcharges that deviate from the live traffic loading, and the PGA.
configurations other than those shown in the Standard Plans, special design walls by Structure Design may be more appropriate.

For the modified design of Standard Plan and Bridge Standard Details sheet retaining walls the Structure Designer will evaluate the lateral sliding and deflection, eccentricity of the resultant foundation load, and internal structural stability requirements.

When the lateral earth pressures resulting from surcharge loads do not conform to those assumed for the Standard Plans and Bridge Standard Details, project specific lateral earth pressures must be developed based on Section 3.11.6 of the AASHTO LRFD Specifications.

**Retaining Walls Supported on Piles (Type 1, Type 5 and Type 7)**

Pile tip elevations for the Strength, Service and Extreme Load demand must be determined according to the Deep Foundation Module. Factored pile load demands will be provided by the Structure Designer and determined on a project specific basis. Pile tip elevations must be provided for the applicable limit states in the format required by *Foundation Reports for Earth Retaining Systems (FR for ERS)*.

Bridge Design Detail Sheets are available for Type 1 SWP, Type 1 SWBP, Type 5 SWP, Type 5 SWBP, Type 7 SWP and Type 7 SWBP. These sheets show the use of driven Class 90 battered piles. Where battered piles are used, the lateral demand on the foundation piles will be resisted by compression of the battered piles.

When vertical piles are required site specific lateral pile analyses are required. The Geoprofessional may provide the Structure Designer with foundation soil parameters to perform the analysis, or the Structure Designer may request that the Geoprofessional perform a lateral pile analysis.

**Type 7 Retaining Walls with Ground Anchors**

Type 7 Retaining Walls use ground anchors to resist overturning, sliding or uplift. The anchor bond zone must be developed below the theoretical shear failure zone for bearing resistance. There is typically at least 5 feet between the bonded zone and the theoretical shear failure surface in the foundation soil or rock. Use a minimum ground anchor unbonded length of 15 feet for both strand and bar tendons (Sabatini et. al.). The minimum horizontal spacing of anchors should be 7 feet.
Ground Improvement

Where existing foundation materials do not provide adequate bearing resistance or result in excessive settlement, consider improving the foundation conditions by removing some or all of the unsuitable material, and replacing it with compacted fill. Material meeting the specification for structure backfill or aggregate base is often used as the replacement material. Consideration should be given to whether a geotechnical fabric is required to separate the backfill from the native soils or to enhance the subgrade behavior. Standard Specification section 19-5.03B discusses a typical configuration that could be used for removal and replacement. Recommend that a typical section of the “remove and replace” be provided in the plans.

Where “remove and replace” is not feasible, consider ground improvement options as an alternative to deep foundations (see Ground Improvement Module).

Although lightweight fill such as cellular concrete, expanded polystyrene (EPS) blocks and volcanic materials (Scoria) may not be considered as ground improvement, they can be used as backfill material behind the conventional retaining wall to reduce the active pressure and to decrease the foundation stresses.

Reporting

Conventional retaining wall recommendations must be reported in either a Geotechnical Design Report (when prepared for the District) or a Foundation Report (when prepared for Structure Design). The 2006 GDR Guidelines are outdated and should not be used as a guide for conventional retaining wall reporting specifics. Instead, use the reporting requirements in Foundation Reports for Earth Retaining Systems to report recommendations regardless of whether the recommendations are conveyed in a GDR or FR.
REFERENCES

1. AASHTO LRFD Bridge Design Specifications, 2012 (Sixth Edition) with California Amendments

2. Caltrans Standard Plans and Revised Standard Plans

3. Caltrans Memo to Designers (MTD) 5-19, *Earth Retaining Systems Communication*


5. Caltrans Geotechnical Manual, *Soil Correlations*


8. Caltrans Geotechnical Manual, *Ground Improvement*
