

James Ralston Resident Engineer

Justin Wood Structure Representative

Contractor Golden State Bridge

Paul Lukaszewicz Vice President GSB



J. Rodgers

The existing bridge was constructed in 1948 and extended on the westerly end in 1961.

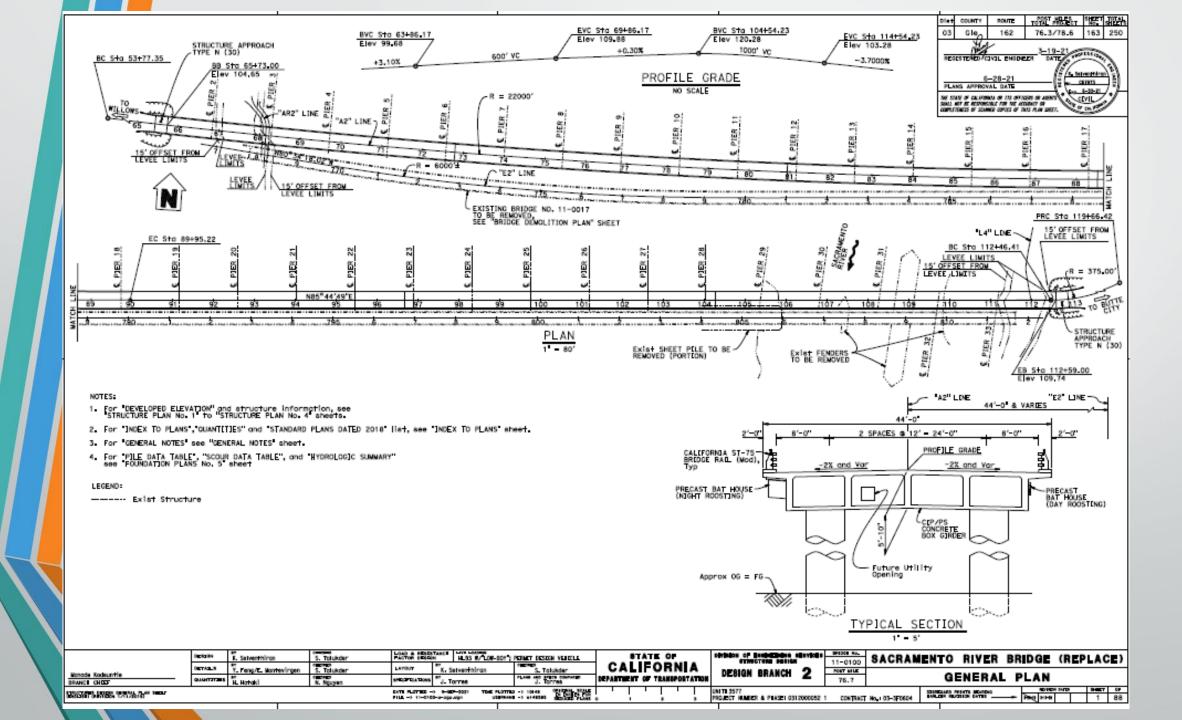
The structure features a steel truss swing bridge and a reinforced concrete viaduct totaling approximately 4,700 feet in length (0.9 miles).

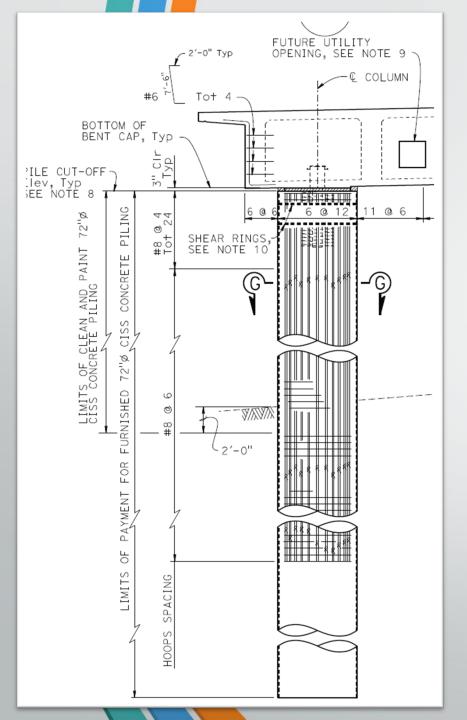
Existing bridge has seismic capacity deficiencies.

Both bridges are passed the 50 year life cycle.

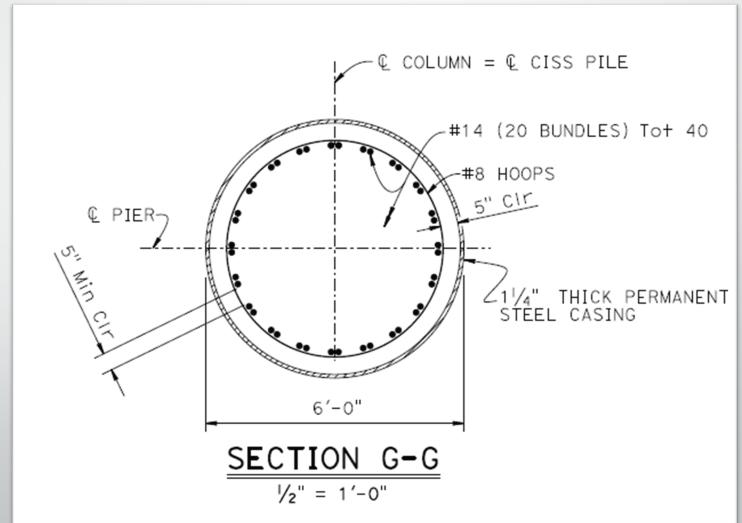
Project is to construct a new bridge (with 12foot lanes and 8-foot shoulders in each direction) on a parallel alignment just north of the existing alignment.

The new bridge will be a cast-in-place prestressed box girder broken up into 6 frames.

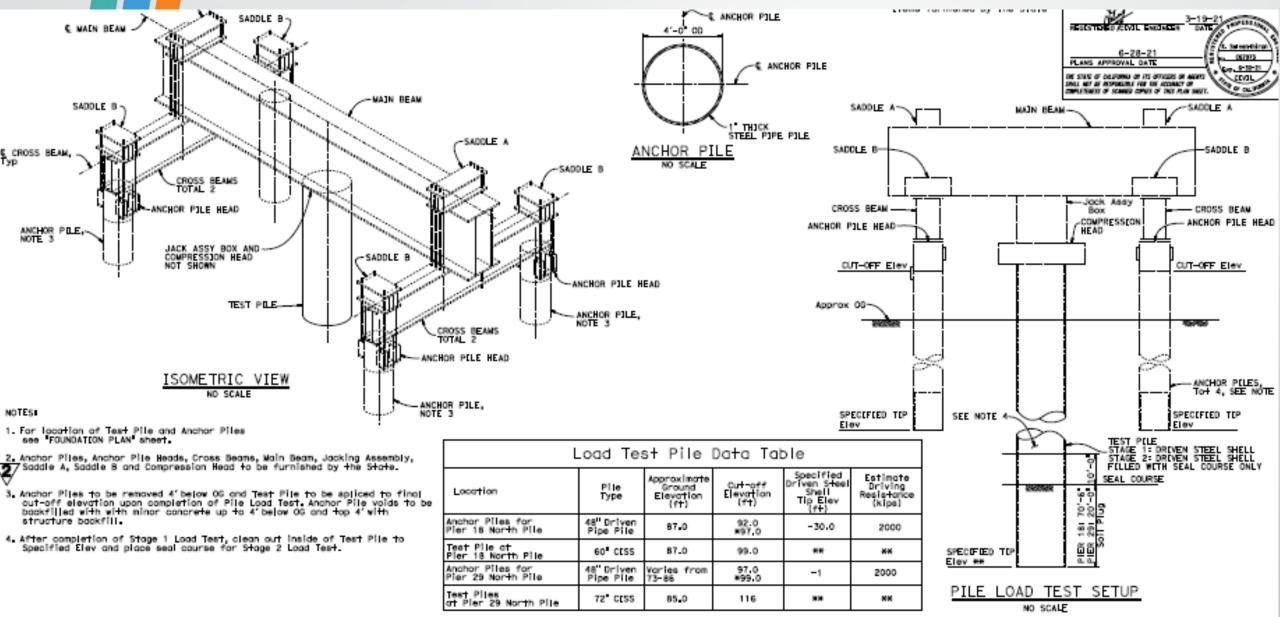




60" & 72" CISS PILES



State Furnished Load Test Beam



Change Order

Force Account

Support Caltrans Foundation Testing to Complete Load Tests

\$440,000 provided in Contract for Supplemental Work

Test Pile Program Drive 48" Anchor Piles





48" Anchor Piles did not reach required capacity

Change Order Extend anchor piles Force Account





Drive 60" and 72" dia Load Test Piles





D180 Diesel Hammer Weight = 160,000 lbs.





Construct Pile Load Test Frames

Construct Pile Load Test Frames

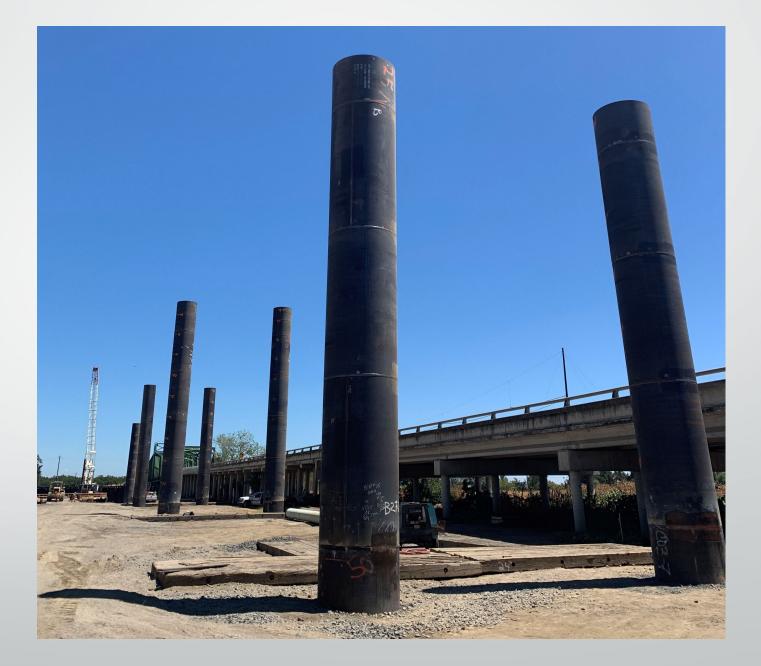


60" and 72" Load Test Piles did not come up to required capacity

Change Order Extend Load Test Piles Force Account Change Order

Allow Contractor to start production piles before Load Test completed

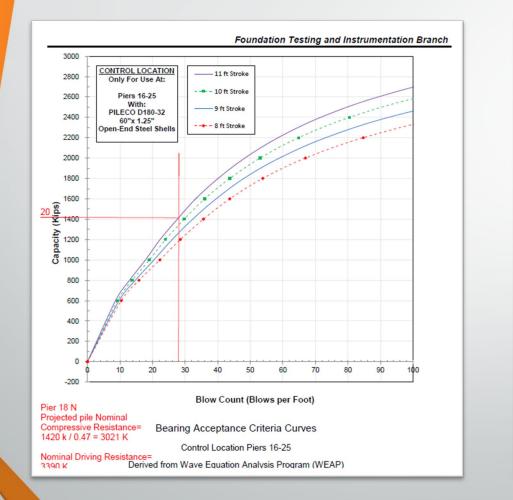
No Cost Deferred Time

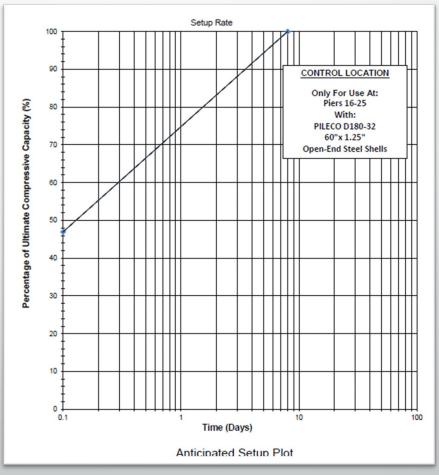




2nd Pile Load Test performed by CT Foundation Testing Branch

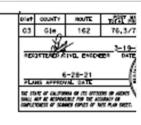
Received Pile Drive Criteria From Foundation Testing Branch





Change Oder Revised Pile Data Table from Geotech Engineer New Tip Elevations

		PILE DATA TABLE Pile Cutoff Nominal Realistonce Design Tip Stevori						(++)	Specified Tip	Required Nonicol	Column	
Location	Pile Type	Pile Cutoff Elevetion (ft)	Compression	Tension	(0)	(b)	(e)	(d)	Specified Tip Elevation (f4)	Required Nominal Driving Resistance (kips)	Tip Elev (1	
Abut 1	CLASS 200 AIT. W	90-4	330	0	37	N/A	58	64	37	330	N/A	
PEER 2 NORTH	CESS 60 ×1.25	83.0	A 3190	0	-5	N/A	23	30	-5 * A	A 3190	35.0	
PEER 2 SOUTH	CESS 60 x1.25"	83.0	A 3200	0	-5	N/A	23	30	-5 * <u>A</u>	A 3200	35.0	
PEER 3 NORTH	CLSS 60 x1.25"	81.0	A 3200	0	-9	N/A	13	34	-9 * <u>A</u>	A 3200	31.0	
PEER 3 SOUTH	CLSS 60"x1.25"	81.0	<u>A</u> 3220	0	-9	N/A	13	34	-9 * <u>A</u>	<u>A</u> 3220	31.0	
PIER 4 NORTH	CLSS 60 ×1.25"	81.0	<u>A</u> 3190	0	1	N/A	26	34	1 * 🔬	<u>A</u> 3190	42.0	
PIER 4 SOUTH	CISS 60 x1 25	81.0	A 3190	0	1	N/A	26	34	1 * 🔬	A 3190	42.0	
PIER 5 NORTH	CESS 60 ×1.25"	0.06	A 3290	0	-9	N/A	9	27	-9 * <u>A</u>	A 3290	27.0	
PIER 5 SOUTH	CESS 60 x1.25	0.06	A 3290	0	-9	N/A	9	27	-9 * <u>A</u>	<u>A</u> 3290	27.0	
PJER 6 NORTH	CLSS 60 x1 25	0.06	<u>A</u> 3430	ô	-14	N/A	9	20	-14 * 🔬	<u>A</u> 3430	25.0	
PJER 6 SOUTH	CLSS 60 ×1.25"	0.06	<u>A</u> 3430	ô	-14	N/A	9	20	-14 × 🔬	<u>A</u> 3430	25.0	
PJER 7 NORTH	CISS 60 ×1.25	82.0	A 3280	0	-9	N/A	14	29	-9 * <u>A</u>	A 3280	27.0	
PIER 7 SOUTH	CESS 60"x1.25"	82.0	A 3280	0	-9	N/A	14	29	-9 × A	A 3260	27.0	
PJER 8 NORTH	CESS 60 x1.25	82.0	A 3150	0	-4	N/A	17	-1	-4 * 🔬	A 3150	29.0	
PIER 8 SOUTH	CLSS 60 x1.25"	82.0	A 3150	0	-4	N/A	17	-1	-4 * 🗛	<u>A</u> 3150	29.0	
PJER 9 NORTH	CLSS 60 x1.25	83.0	<u>A</u> 3180	0	-12	N/A	13	34	-12 * <u>A</u>	<u>A</u> 3160	30.0	
PIER 9 SOUTH	CLSS 60 x1.25	83.0	<u>A</u> 3180	0	-12	N/A	13	34	-12 × 🔬	A 3180	30.0	
PJER 10 NORTH	CESS 60 ×1.25	83.0	A 3150	0	-11	N/A	14	31	-11 × 🔬	A 3150	31.0	
PJER 10 SOUTH	CESS 60 x1.25	83.0	A 3150	0	-11	N/A	14	31	-11 * <u>A</u>	<u>A</u> 3150	31.0	
PJER 11 NORTH	CLSS 60 ×1.25	84.0	A 3270	0	-7	N/A	20	30	-7 * <u>A</u>	<u>A</u> 3270	34.0	
PJER 11 SOUTH	CLSS 60 ×1.25"	84.0	A 3270	0	-7	N/A	20	30	-7 * <u>A</u>	<u>A</u> 3270	34.0	
PIER 12 NORTH	CLSS 60 ×1.25	84_0	<u>A</u> 3400	0	-13	N/A	8	34	-13 × 🔬	<u>A</u> 3400	27.0	
PJER 12 SOUTH	CLSS 60 ×1.25	84.0	A 3400	0	-13	N/A	8	34	-13 × 🔬	<u>A</u> 3400	27.0	
PJER 13 NORTH	CESS 60 x1.25	84.0	A 3270	0	-1	N/A	16	36	-4 * <u>A</u>	<u>A</u> 3270	33.0	
PIER 13 SOUTH	CESS 60 ×1.25	84.0	A 3270	0	-4	N/A	16	36	-4 * <u>A</u>	<u>A</u> 3270	33.0	
PJER 14 NORTH	CLSS 60 ×1.25"	84.0	A 3160	0	-3	N/A	16	35	-3 * <u>A</u>	<u>A</u> 3160	33.0	
PIER 14 SOUTH	CLSS 60 ×1.25	84_0	<u>A</u> 3180	0	-3	N/A	16	35	-3 * <u>A</u>	<u>A</u> 3160	33.0	
DER 15 NORTH	CLSS 60 ×1.25	84.0	A 3180	0	-7	N/A	16	34	-7 = 🔬	<u>A</u> 3180	31.0	
PIER 15 SOUTH	CESS 60 ×1.25	84.0	A 3160	0	-7	N/A	16	34	-7 * <u>A</u>	A 3180	31.0	
PJER 16 NORTH	CESS 60 ×1.25	84.0	A 3190	0	<u>A</u> -90	N/A	-7	26	<u>A</u> -90	<u>A</u> 3190	18.5	
PJER 16 SOUTH	CESS 60 x1.25	0.48	A 3190	0	<u>A</u> −90	N/A	-7	26	A -90	<u>A</u> 3190	18.5	
PIER 17 NORTH	CLSS 60 ×1.25"	84.0	<u>A</u> 3300	0	A -25	N/A	-12	29	A -95	<u>A</u> 3300	19.0	
PIER 17 SOUTH	CCSS 60 ×1.25	84_0	<u>A</u> 3300	0	<u>A</u> -95	N/A	-12	29	<u>A</u> -95	A 3300	19.0	
PIER 18 NORTH	CESS 60 ×1.25	84.0	A 3390	0	<u>A</u> -113	N/A	-19	11	<u>A</u> -113	A 3390	14.5	
PIER 18 SOUTH	CESS 60 ×1.25	84.0	▲ 3390	0	<u>A</u> -113	N/A	-19	11	<u>A</u> -113	<u>A</u> 3390	14.5	
PJER 19 NORTH	CLSS 60"x1.25"	84.0	A 3440	0	A-110	N/A	-9	15	A-110	<u>A</u> 3440	15.0	
PIER 19 SOUTH	CLSS 60 ×1.25"	84.0	<u>A</u> 3440	0	<u>A</u> -110	N/A	-9	15	A-110	<u>A</u> 3440	15.0	
PIER 20 NORTH	CLSS 60 x1.25"	84_0	<u>A</u> 3670	0	<u>A</u> -110	N/A	-1	11	<u>A</u> -110	<u>A</u> 3670	10.5	
PIER 20 SOUTH	CESS 60 ×1.25	84.0	A 3670	0	<u>A</u> -110	N/A	-1	11	<u>A-110</u>	<u>A</u> 3670	10.5	
PJER 21 NORTH	CESS 60 x1.25"	84.0	A 3520	0	<u>A</u> -108	N/A	-4	11	<u>A</u> -108	A 3520	10.5	



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NOTES:

Change Oder Revised Pile Data Table from Geotech Engineer – New Tip Elevations

Clay Zone: Added 50 ft to each 60" pile from Pier 16 to Pier 25 (20 piles total)

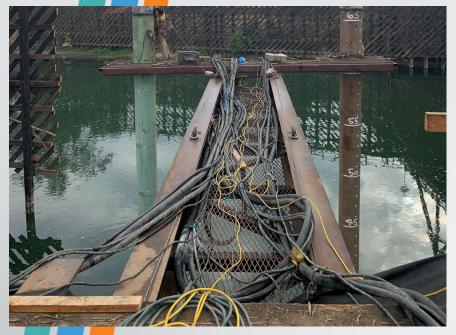
Silty Sandy Gravel Zone: Added 10 ft to piles from Pier 2 to Pier 15 and Pier 33 (30 piles total)

Total estimated cost to extend piles = \$7.4 Million Added 10% cost to entire project.





Go Forward With Building a Bridge

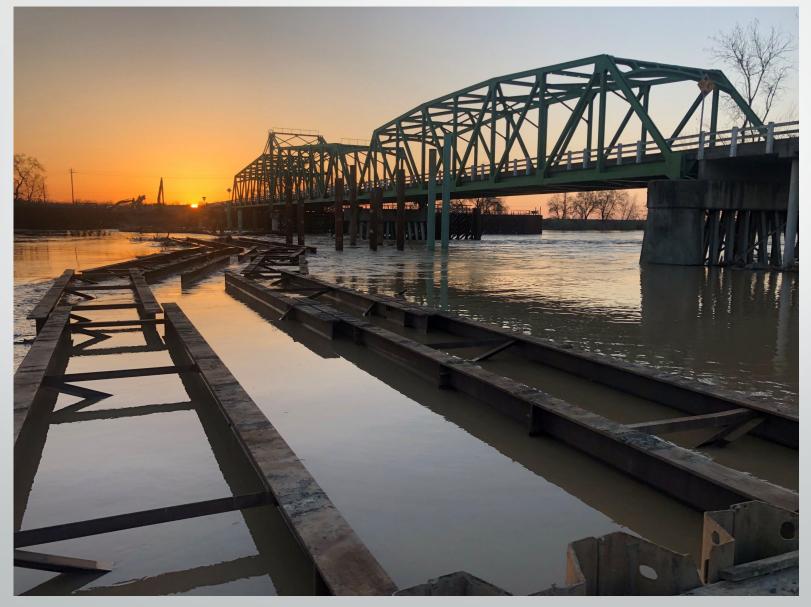






Go Forward With Building a Bridge

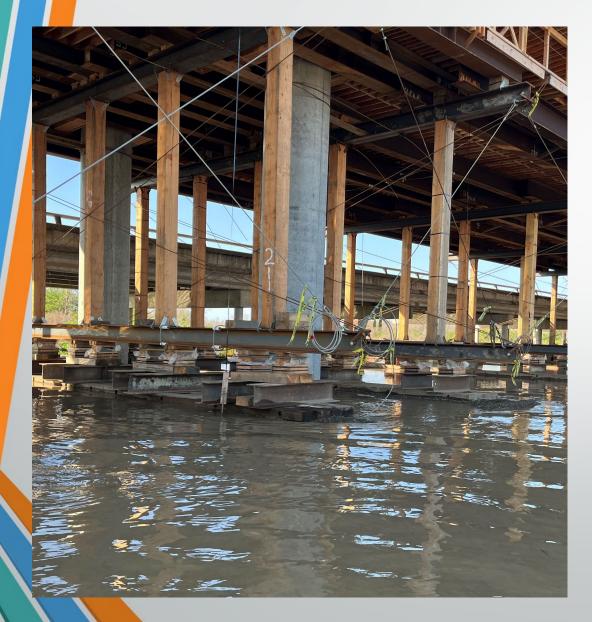
Sacramento River flooding – January 2023

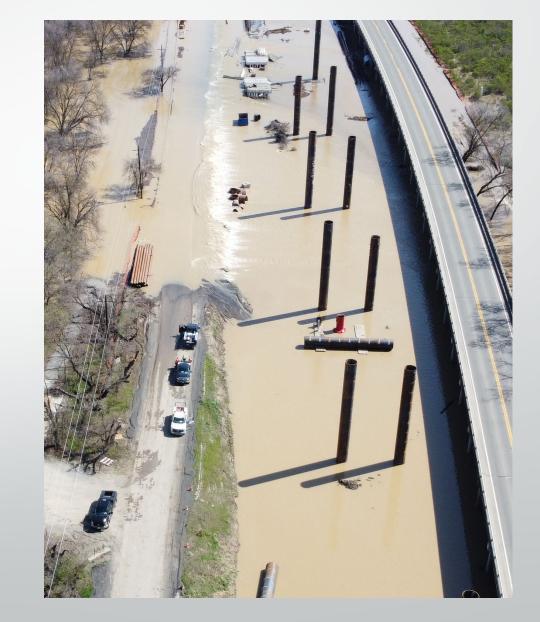


Sacramento River Flooding – March 2023



Sacramento River Flooding – March 2023





Frames 4 & 5 looking east



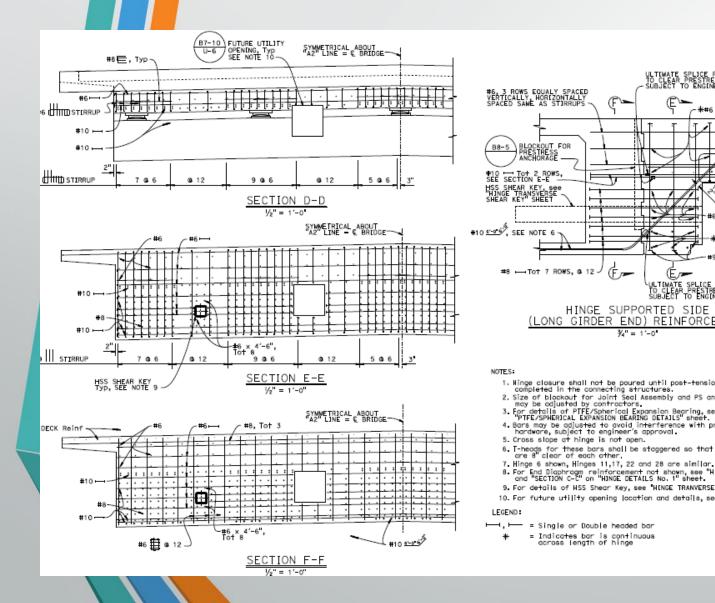
Frames 4 & 5 looking west

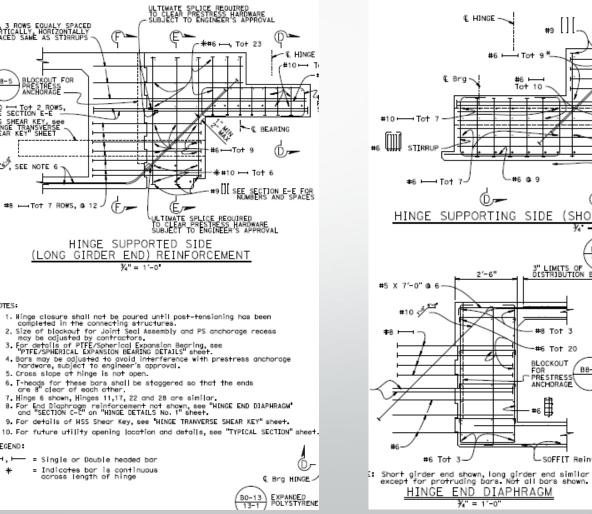


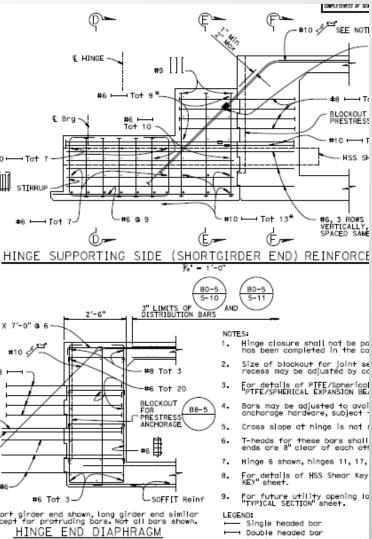
Hinge Details

(E -

¾" = 1'-0"

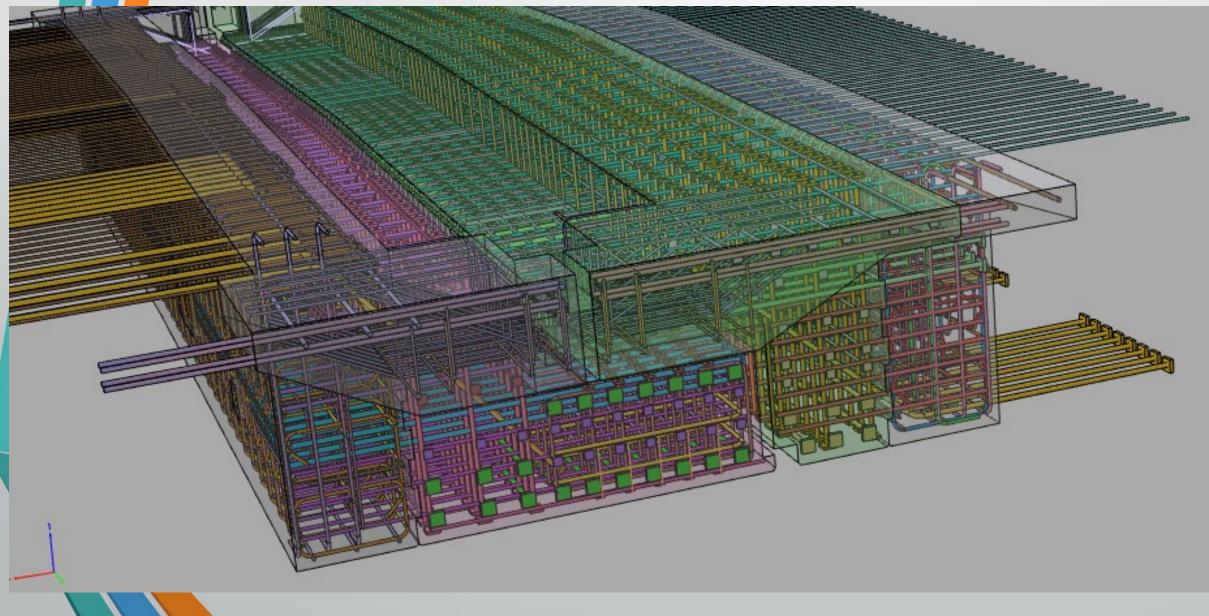




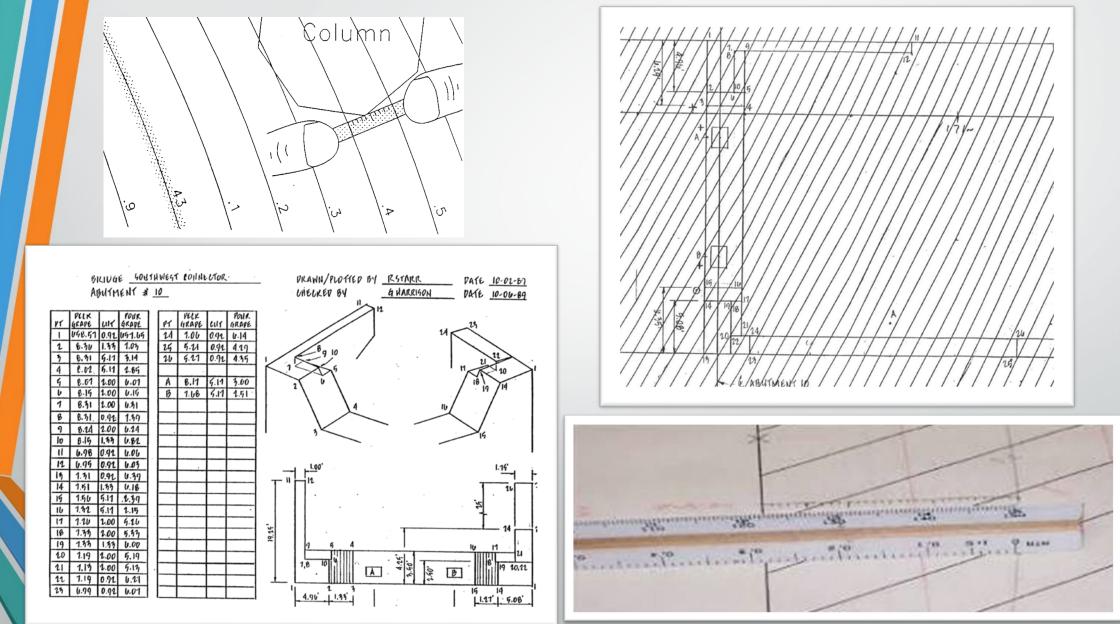


* Bar is continuous across ler

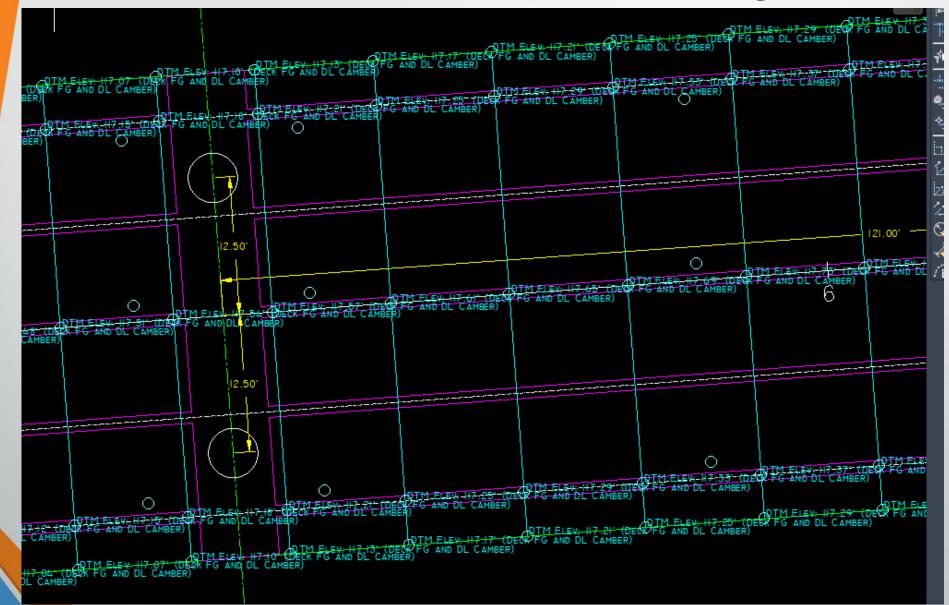
3D Modeling of Hinge



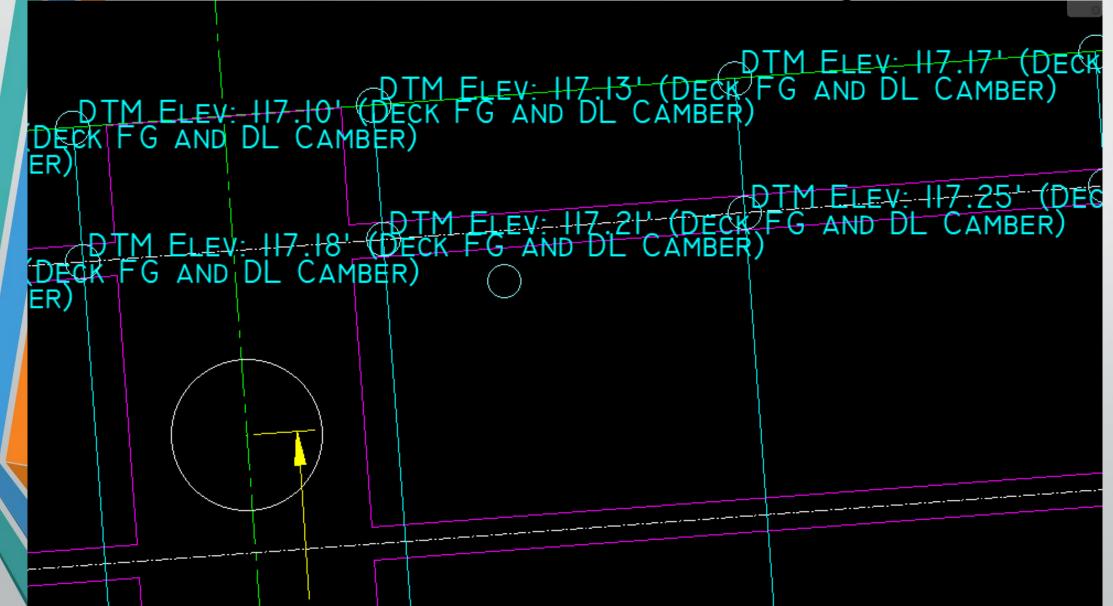
Picking Grades from 4-Scales



Civil 3D Surface Modeling



Civil 3D Surface Modeling



On schedule to finish bridge work Fall 2025

Plant Establishment finish November 2026.

Questions?